

Supplementary information for:

Optimized ‘Detectors’ for dynamics analysis in solid-state NMR

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I. Glossary of terms

| Name | Symbol | Units | Description |
|---------------------------------|-----------------------------------|-----------------|---|
| <i>Distribution of motion</i> | $(1-S^2)\theta(z)$ | unitless | Describes how motion is distributed as a function of correlation time, where $z = \log_{10}(\tau_c/1 \text{ s})$. $(1-S^2)$ gives the total amplitude of motion, so that $\theta(z)$ always integrates to one. |
| <i>Relaxation rate constant</i> | $R_\zeta^{(\theta,S)}$ | s^{-1} | The relaxation-rate constant obtained under experimental conditions denoted by ζ , for a distribution of motion $(1-S^2)\theta(z)$. May be obtained by integrating the product of the sensitivity of that rate constant, $R_\zeta(z)$, times the distribution of motion, $(1-S^2)\theta(z)$. |
| <i>Sensitivity</i> | $R_\zeta(z)$ | s^{-1} | The relaxation rate constant obtained under experimental conditions denoted by ζ , for a mono-exponential correlation function, having correlation time $\tau_c = 10^z \text{ s}$, and amplitude $1-S^2 = 1$. |
| <i>Detector</i> | – | – | A mathematical tool used to quantify the amount of motion for a range of correlation times. |
| <i>Detector sensitivity</i> | $\rho_n(z)$ | unitless | Defines how a detector responds to a particular correlation time, $\tau_c = 10^z \text{ s}$. Its value as a function of z is obtained by taking a linear combination of rate constant sensitivities (using the same linear combination as is used to obtain the detector responses). |
| <i>Detector response</i> | $\rho_n^{(\theta,S)}$ | unitless | A quantity, describing the amount of motion for a particular range of correlation times, rigorously defined as the integral of the product of the detector sensitivity, $\rho_n(z)$, and the distribution of motion, $(1-S^2)\theta(z)$. Obtained by taking an appropriate linear combination of experimental rate constants (strictly speaking, by fitting a vector of the rate constants to the detection vectors, \vec{r}_n). |
| <i>Normalized rate constant</i> | $\mathfrak{R}_\zeta^{(\theta,S)}$ | unitless | The relaxation rate constant divided by some normalization constant, c_ζ , to yield a dimensionless relaxation rate constant. Here, $c_\zeta = \max(R_\zeta(z))$. |
| <i>Allowed region</i> | – | – | For a given set of experiments, the allowed region is all sets of rate constants ($R_\zeta^{(\theta,S)}$) that can be obtained for any arbitrary distribution of motion, given by $(1-S^2)\theta(z)$. |
| <i>Detection vector</i> | \vec{r}_n | s^{-1} | A vector containing carefully chosen values of the $R_\zeta^{(\theta,S)}$, so that a vector containing the full set of experimentally determined relaxation rate constants is assumed to be a linear combination of all detection vectors, given by $\rho_1^{(\theta,S)}\vec{r}_1 + \rho_2^{(\theta,S)}\vec{r}_2 + \dots$. |

| | | | |
|---|--|-----------------------|---|
| <i>Sum of normalized rate constants</i> | $\sum_{\zeta} \mathfrak{R}_{\zeta}^{(\theta,S)}$ | unitless | Sum of all normalized rate constants for an experimental data set, used for calculating the ratio of rates. |
| <i>Ratio of rates</i> | κ_{ζ} | unitless | For experimental conditions denoted by ζ , this is the ratio of the normalized rate constants, $\mathfrak{R}_{\zeta}^{(\theta,S)}$, divided by the sum of normalized rate constants, $\sum \mathfrak{R}^{(\theta,S)}$, which is used for defining positions in the reduced space. |
| <i>Reduced space</i> | – | – | For a set of experiments, the reduced space is defined by the ratios of rates, κ_{ζ} , for that set of experiments. The dimensionality of this space is one less than the number of experiments- achieved by omitting one of the experiments when calculating the κ_{ζ} . |
| <i>Reduced vector</i> | $\vec{\kappa}$ | unitless | Vector of ratios of rates, κ_{ζ} , defining a position in the reduced space. These positions can be used to define detection vectors, although note that the reduced vector only defines the direction of the detection vector, but not the length. |
| <i>Effective width</i> | Δz_n | unitless (vs. 1 s) | The effective width of a detector is defined as the detector integral divided by its maximum, given on a base-10 log scale. $\Delta z = \int \rho_n(z) dz / \max(\rho_n(z))$ |
| <i>Detector center</i> | z_n^0 | unitless (vs. 1 s) | This gives the center of the detector sensitivity, on a logarithmic scale (unitless, with reference to 1 s using a base-10 log). Defined as follows: $z_n^0 = \int z \rho_n(z) dz / \int \rho_n(z) dz$ |

II. Detector analysis results for Ubiquitin

Table I: Detector analysis results for Ubiquitin. $\rho_n^{(\theta,S)}$ gives the best fit value, and the + and – columns 95% confidence interval as deviations from the best fit value (see text Fig. 12). Original experimental data is found in references [1,2].

| Residue | $\rho_0^{(\theta,S)}$ | + | – | $\rho_1^{(\theta,S)}$ | + | – | $\rho_2^{(\theta,S)}$ | + | – |
|---------|-----------------------|--------|--------|-----------------------|--------|--------|-----------------------|--------|--------|
| 2 | 0.1209 | 0.0242 | 0.0231 | 0.0220 | 0.0106 | 0.0142 | 0.0228 | 0.0150 | 0.0120 |
| 3 | 0.1269 | 0.0199 | 0.0192 | 0.0073 | 0.0032 | 0.0034 | 0.0054 | 0.0032 | 0.0038 |
| 4 | 0.9836 | 0.0164 | 1.5421 | 0.0002 | 0.0032 | 0.0002 | 0.0137 | 0.0014 | 0.0057 |
| 6 | 0.9960 | 0.0039 | 1.5546 | 0.0000 | 1.0000 | 0.0000 | 0.0000 | 1.0000 | 0.0000 |
| 7 | 0.1189 | 0.0220 | 0.6774 | 0.0000 | 0.0172 | 0.0000 | 0.0451 | 0.0056 | 0.0259 |
| 9 | 0.9635 | 0.0364 | 1.5221 | 0.0000 | 1.0000 | 0.0000 | 0.0000 | 1.0000 | 0.0000 |
| 10 | 0.1102 | 0.0529 | 0.0495 | 0.0847 | 0.0092 | 0.0355 | 0.0000 | 0.0293 | 0.0000 |
| 11 | 0.0764 | 0.0677 | 0.1086 | 0.2952 | 0.0471 | 0.2155 | 0.0000 | 0.2544 | 0.0000 |
| 12 | 0.1111 | 0.0302 | 0.0323 | 0.0075 | 0.0434 | 0.0075 | 0.0417 | 0.0144 | 0.0417 |
| 13 | 0.9946 | 0.0053 | 1.5532 | 0.0000 | 1.0000 | 0.0000 | 0.0000 | 1.0000 | 0.0000 |
| 14 | 0.9959 | 0.0041 | 1.5544 | 0.0000 | 1.0000 | 0.0000 | 0.0000 | 1.0000 | 0.0000 |
| 15 | 0.1127 | 0.0155 | 0.0192 | 0.0149 | 0.0033 | 0.0031 | 0.0077 | 0.0027 | 0.0030 |
| 16 | 0.1621 | 0.0222 | 0.0244 | 0.0324 | 0.0047 | 0.0065 | 0.0041 | 0.0060 | 0.0041 |
| 17 | 0.9698 | 0.0302 | 1.5283 | 0.0169 | 0.0056 | 0.0071 | 0.0088 | 0.0083 | 0.0079 |
| 18 | 0.9964 | 0.0035 | 1.5550 | 0.0000 | 1.0000 | 0.0000 | 0.0000 | 1.0000 | 0.0000 |
| 20 | 0.1406 | 0.0407 | 0.0374 | 0.0271 | 0.0019 | 0.0083 | 0.0010 | 0.0067 | 0.0010 |
| 21 | 0.1203 | 0.0192 | 0.0247 | 0.0086 | 0.0030 | 0.0029 | 0.0059 | 0.0035 | 0.0035 |
| 22 | 0.1378 | 0.0454 | 0.0444 | 0.0081 | 0.0026 | 0.0050 | 0.0016 | 0.0048 | 0.0016 |
| 23 | 0.1104 | 0.0227 | 0.0223 | 0.0108 | 0.0052 | 0.0098 | 0.0037 | 0.0074 | 0.0037 |
| 24 | 0.9767 | 0.0233 | 1.5352 | 0.0000 | 1.0000 | 0.0000 | 0.0000 | 1.0000 | 0.0000 |
| 25 | 0.9878 | 0.0122 | 1.5463 | 0.0000 | 1.0000 | 0.0000 | 0.0000 | 1.0000 | 0.0000 |
| 26 | 0.1052 | 0.0323 | 0.0319 | 0.0015 | 0.0033 | 0.0015 | 0.0121 | 0.0022 | 0.0036 |
| 27 | 0.1025 | 0.0473 | 0.0560 | 0.0010 | 0.0069 | 0.0010 | 0.0123 | 0.0037 | 0.0085 |
| 29 | 0.9747 | 0.0253 | 1.5332 | 0.0000 | 0.0120 | 0.0000 | 0.0231 | 0.0034 | 0.0231 |
| 30 | 0.1146 | 0.0417 | 0.0335 | 0.0000 | 0.0039 | 0.0000 | 0.0175 | 0.0018 | 0.0064 |
| 31 | 0.1105 | 0.0938 | 0.0931 | 0.0000 | 0.0046 | 0.0000 | 0.0107 | 0.0012 | 0.0045 |
| 32 | 0.1090 | 0.0389 | 0.0402 | 0.0000 | 0.0022 | 0.0000 | 0.0099 | 0.0013 | 0.0040 |
| 33 | 0.1246 | 0.0422 | 0.0492 | 0.0166 | 0.0048 | 0.0060 | 0.0041 | 0.0053 | 0.0041 |
| 34 | 0.0969 | 0.0441 | 0.0442 | 0.0059 | 0.0037 | 0.0041 | 0.0185 | 0.0051 | 0.0059 |
| 35 | 0.0720 | 0.0389 | 0.0416 | 0.0000 | 0.0057 | 0.0000 | 0.0252 | 0.0022 | 0.0109 |
| 36 | 0.2406 | 0.0275 | 0.0327 | 0.0262 | 0.0036 | 0.0040 | 0.0058 | 0.0046 | 0.0047 |
| 39 | 0.1281 | 0.0275 | 0.0327 | 0.0131 | 0.0191 | 0.0131 | 0.0310 | 0.0184 | 0.0249 |
| 40 | 0.1227 | 0.0405 | 0.0461 | 0.0185 | 0.0059 | 0.0051 | 0.0122 | 0.0064 | 0.0074 |
| 41 | 0.1455 | 0.0362 | 0.0401 | 0.0201 | 0.0063 | 0.0064 | 0.0059 | 0.0063 | 0.0059 |
| 42 | 0.1119 | 0.0281 | 0.0323 | 0.0000 | 0.0072 | 0.0000 | 0.0229 | 0.0026 | 0.0129 |
| 43 | 0.1055 | 0.0272 | 0.0264 | 0.0195 | 0.0025 | 0.0175 | 0.0000 | 0.0136 | 0.0000 |
| 44 | 0.1034 | 0.0182 | 0.0151 | 0.0064 | 0.0034 | 0.0037 | 0.0086 | 0.0047 | 0.0041 |

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|----|---------|--------|--------|--------|--------|--------|--------|--------|--------|
| 45 | 0.1118 | 0.0206 | 0.0235 | 0.0010 | 0.0063 | 0.0010 | 0.0112 | 0.0039 | 0.0112 |
| 46 | 0.0952 | 0.0358 | 0.0441 | 0.0125 | 0.0029 | 0.0048 | 0.0027 | 0.0057 | 0.0027 |
| 47 | 0.1269 | 0.0343 | 0.0348 | 0.0227 | 0.0043 | 0.0059 | 0.0058 | 0.0054 | 0.0050 |
| 48 | 0.1499 | 0.0364 | 0.0361 | 0.0305 | 0.0058 | 0.0052 | 0.0075 | 0.0074 | 0.0075 |
| 49 | 0.1379 | 0.0280 | 0.0328 | 0.0202 | 0.0038 | 0.0045 | 0.0069 | 0.0050 | 0.0049 |
| 51 | 0.0988 | 0.0318 | 0.0367 | 0.0022 | 0.0123 | 0.0022 | 0.0389 | 0.0051 | 0.0162 |
| 52 | 0.1730 | 0.0256 | 0.0295 | 0.0284 | 0.0060 | 0.0060 | 0.0190 | 0.0075 | 0.0077 |
| 54 | 0.1769 | 0.0330 | 0.0304 | 0.0235 | 0.0072 | 0.0076 | 0.0104 | 0.0070 | 0.0079 |
| 55 | 0.1419 | 0.0228 | 0.0235 | 0.0130 | 0.0037 | 0.0049 | 0.0033 | 0.0036 | 0.0033 |
| 56 | 0.1233 | 0.0246 | 0.0210 | 0.0000 | 0.0066 | 0.0000 | 0.0108 | 0.0021 | 0.0108 |
| 57 | 0.9957 | 0.0043 | 1.5542 | 0.0000 | 1.0000 | 0.0000 | 0.0000 | 1.0000 | 0.0000 |
| 58 | 0.1093 | 0.0436 | 0.0412 | 0.0054 | 0.0030 | 0.0026 | 0.0087 | 0.0025 | 0.0031 |
| 59 | 0.1412 | 0.0287 | 0.0292 | 0.0068 | 0.0039 | 0.0040 | 0.0108 | 0.0043 | 0.0049 |
| 60 | 0.1154 | 0.0380 | 0.0449 | 0.0102 | 0.0041 | 0.0042 | 0.0140 | 0.0055 | 0.0066 |
| 61 | 0.1483 | 0.0300 | 0.0292 | 0.0182 | 0.0020 | 0.0093 | 0.0004 | 0.0074 | 0.0004 |
| 62 | -0.1044 | 0.2602 | 0.4541 | 0.0049 | 0.0032 | 0.0036 | 0.0198 | 0.0042 | 0.0038 |
| 63 | 0.1571 | 0.0194 | 0.0263 | 0.0111 | 0.0039 | 0.0058 | 0.0058 | 0.0093 | 0.0058 |
| 64 | 0.1048 | 0.0208 | 0.6633 | 0.0000 | 0.0059 | 0.0000 | 0.0292 | 0.0008 | 0.0064 |
| 65 | 0.1756 | 0.0287 | 0.0407 | 0.0036 | 0.0024 | 0.0023 | 0.0089 | 0.0034 | 0.0042 |
| 66 | 0.9978 | 0.0022 | 1.5563 | 0.0000 | 1.0000 | 0.0000 | 0.0000 | 1.0000 | 0.0000 |
| 67 | 0.9977 | 0.0023 | 1.5562 | 0.0000 | 1.0000 | 0.0000 | 0.0000 | 1.0000 | 0.0000 |
| 68 | 0.1281 | 0.0453 | 0.0454 | 0.0062 | 0.0029 | 0.0047 | 0.0031 | 0.0075 | 0.0031 |
| 69 | 0.9973 | 0.0027 | 1.5558 | 0.0000 | 1.0000 | 0.0000 | 0.0000 | 1.0000 | 0.0000 |
| 70 | 0.0999 | 0.0174 | 0.0157 | 0.0158 | 0.0045 | 0.0053 | 0.0046 | 0.0058 | 0.0046 |
| 71 | 0.9863 | 0.0137 | 1.5448 | 0.0000 | 1.0000 | 0.0000 | 0.0000 | 1.0000 | 0.0000 |

Table 1 cont.

| Residue | $\rho_3^{(\theta,S)}$ | + | - | $\rho_4^{(\theta,S)}$ | + | - |
|---------|-----------------------|--------|--------|-----------------------|--------|--------|
| 2 | 0.0042 | 0.0004 | 0.0004 | 0.0020 | 0.0003 | 0.0003 |
| 3 | 0.0029 | 0.0002 | 0.0002 | 0.0014 | 0.0002 | 0.0002 |
| 4 | 0.0015 | 0.0001 | 0.0001 | 0.0010 | 0.0002 | 0.0001 |
| 6 | 0.0026 | 0.0001 | 0.0001 | 0.0014 | 0.0001 | 0.0002 |
| 7 | 0.0000 | 0.6970 | 0.0000 | 0.0000 | 0.6978 | 0.0000 |
| 9 | 0.0111 | 0.0160 | 0.0111 | 0.0254 | 0.0120 | 0.0177 |
| 10 | 0.0165 | 0.0030 | 0.0050 | 0.0116 | 0.0048 | 0.0042 |
| 11 | 0.0230 | 0.0044 | 0.0047 | 0.0054 | 0.0036 | 0.0031 |
| 12 | 0.0066 | 0.0015 | 0.0017 | 0.0030 | 0.0015 | 0.0020 |
| 13 | 0.0040 | 0.0003 | 0.0003 | 0.0014 | 0.0003 | 0.0003 |
| 14 | 0.0027 | 0.0001 | 0.0002 | 0.0014 | 0.0001 | 0.0001 |
| 15 | 0.0018 | 0.0001 | 0.0001 | 0.0009 | 0.0001 | 0.0001 |
| 16 | 0.0023 | 0.0002 | 0.0001 | 0.0011 | 0.0001 | 0.0002 |
| 17 | 0.0029 | 0.0007 | 0.0006 | 0.0017 | 0.0013 | 0.0016 |
| 18 | 0.0027 | 0.0002 | 0.0002 | 0.0009 | 0.0003 | 0.0002 |
| 20 | 0.0042 | 0.0005 | 0.0004 | 0.0041 | 0.0007 | 0.0008 |

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|----|--------|--------|--------|--------|--------|--------|
| 21 | 0.0021 | 0.0001 | 0.0001 | 0.0021 | 0.0002 | 0.0001 |
| 22 | 0.0017 | 0.0002 | 0.0002 | 0.0018 | 0.0002 | 0.0002 |
| 23 | 0.0016 | 0.0002 | 0.0003 | 0.0014 | 0.0002 | 0.0002 |
| 24 | 0.0139 | 0.0077 | 0.0075 | 0.0094 | 0.0060 | 0.0067 |
| 25 | 0.0077 | 0.0025 | 0.0031 | 0.0045 | 0.0043 | 0.0042 |
| 26 | 0.0010 | 0.0001 | 0.0001 | 0.0012 | 0.0001 | 0.0001 |
| 27 | 0.0010 | 0.0001 | 0.0001 | 0.0012 | 0.0001 | 0.0001 |
| 29 | 0.0014 | 0.0001 | 0.0001 | 0.0009 | 0.0001 | 0.0001 |
| 30 | 0.0011 | 0.0001 | 0.0001 | 0.0008 | 0.0001 | 0.0001 |
| 31 | 0.0017 | 0.0001 | 0.0010 | 0.0000 | 0.0020 | 0.0000 |
| 32 | 0.0010 | 0.0001 | 0.0002 | 0.0011 | 0.0001 | 0.0001 |
| 33 | 0.0016 | 0.0002 | 0.0002 | 0.0011 | 0.0002 | 0.0002 |
| 34 | 0.0023 | 0.0002 | 0.0001 | 0.0013 | 0.0001 | 0.0001 |
| 35 | 0.0024 | 0.0002 | 0.0002 | 0.0014 | 0.0001 | 0.0002 |
| 36 | 0.0036 | 0.0005 | 0.0004 | 0.0018 | 0.0005 | 0.0006 |
| 39 | 0.0030 | 0.0003 | 0.0003 | 0.0018 | 0.0003 | 0.0003 |
| 40 | 0.0051 | 0.0009 | 0.0007 | 0.0055 | 0.0009 | 0.0012 |
| 41 | 0.0052 | 0.0006 | 0.0006 | 0.0044 | 0.0004 | 0.0005 |
| 42 | 0.0028 | 0.0001 | 0.0001 | 0.0014 | 0.0001 | 0.0001 |
| 43 | 0.0025 | 0.0001 | 0.0001 | 0.0015 | 0.0001 | 0.0001 |
| 44 | 0.0013 | 0.0001 | 0.0001 | 0.0013 | 0.0001 | 0.0001 |
| 45 | 0.0011 | 0.0001 | 0.0001 | 0.0009 | 0.0001 | 0.0001 |
| 46 | 0.0015 | 0.0001 | 0.0001 | 0.0011 | 0.0001 | 0.0001 |
| 47 | 0.0025 | 0.0001 | 0.0001 | 0.0011 | 0.0001 | 0.0001 |
| 48 | 0.0019 | 0.0002 | 0.0002 | 0.0012 | 0.0002 | 0.0002 |
| 49 | 0.0028 | 0.0001 | 0.0001 | 0.0012 | 0.0002 | 0.0002 |
| 51 | 0.0037 | 0.0004 | 0.0003 | 0.0025 | 0.0003 | 0.0004 |
| 52 | 0.0052 | 0.0004 | 0.0004 | 0.0035 | 0.0004 | 0.0005 |
| 54 | 0.0021 | 0.0001 | 0.0001 | 0.0022 | 0.0001 | 0.0001 |
| 55 | 0.0021 | 0.0004 | 0.0003 | 0.0017 | 0.0003 | 0.0004 |
| 56 | 0.0010 | 0.0001 | 0.0001 | 0.0009 | 0.0001 | 0.0001 |
| 57 | 0.0025 | 0.0003 | 0.0003 | 0.0018 | 0.0004 | 0.0002 |
| 58 | 0.0014 | 0.0001 | 0.0001 | 0.0012 | 0.0002 | 0.0002 |
| 59 | 0.0016 | 0.0002 | 0.0002 | 0.0016 | 0.0002 | 0.0002 |
| 60 | 0.0023 | 0.0001 | 0.0001 | 0.0011 | 0.0001 | 0.0001 |
| 61 | 0.0019 | 0.0001 | 0.0001 | 0.0012 | 0.0001 | 0.0001 |
| 62 | 0.0000 | 0.7187 | 0.0000 | 0.2447 | 0.4746 | 0.2447 |
| 63 | 0.0029 | 0.0009 | 0.0009 | 0.0010 | 0.0008 | 0.0009 |
| 64 | 0.0000 | 0.6875 | 0.0000 | 0.0000 | 0.6874 | 0.0000 |
| 65 | 0.0019 | 0.0001 | 0.0001 | 0.0010 | 0.0001 | 0.0001 |
| 66 | 0.0015 | 0.0001 | 0.0001 | 0.0008 | 0.0001 | 0.0001 |
| 67 | 0.0013 | 0.0001 | 0.0000 | 0.0010 | 0.0001 | 0.0001 |
| 68 | 0.0022 | 0.0005 | 0.0005 | 0.0014 | 0.0006 | 0.0006 |
| 69 | 0.0016 | 0.0001 | 0.0001 | 0.0012 | 0.0001 | 0.0001 |
| 70 | 0.0043 | 0.0003 | 0.0003 | 0.0014 | 0.0003 | 0.0003 |

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|----|--------|--------|--------|--------|--------|--------|
| 71 | 0.0089 | 0.0021 | 0.0021 | 0.0048 | 0.0022 | 0.0023 |
|----|--------|--------|--------|--------|--------|--------|

Table II. Detectors calculated from explicit models (text Fig. 13). Original analyses are found in references [1,2].

| Residue | $\rho_0^{(\theta,S)}$ | $\rho_1^{(\theta,S)}$ | $\rho_2^{(\theta,S)}$ | $\rho_3^{(\theta,S)}$ | $\rho_4^{(\theta,S)}$ |
|---------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|
| 2 | 0.1188 | 0.0224 | 0.0223 | 0.0048 | 0.0020 |
| 3 | 0.1257 | 0.0082 | 0.0062 | 0.0034 | 0.0014 |
| 5 | 0.1227 | 0.0121 | 0.0005 | 0.0019 | 0.0010 |
| 7 | 0.1142 | 0.0005 | 0.0457 | 0.0029 | 0.0014 |
| 10 | 0.1309 | 0.0698 | 0.0148 | 0.0182 | 0.0114 |
| 11 | 0.0630 | 0.2617 | 0.0399 | 0.0247 | 0.0040 |
| 12 | 0.1180 | 0.0067 | 0.0438 | 0.0074 | 0.0030 |
| 14 | 0.1235 | 0.0066 | 0.1006 | 0.0045 | 0.0013 |
| 15 | 0.1107 | 0.0153 | 0.0070 | 0.0040 | 0.0017 |
| 16 | 0.1637 | 0.0328 | 0.0041 | 0.0017 | 0.0008 |
| 18 | 0.1390 | 0.0152 | 0.0005 | 0.0024 | 0.0010 |
| 20 | 0.1337 | 0.0266 | 0.0015 | 0.0046 | 0.0044 |
| 21 | 0.1161 | 0.0083 | 0.0058 | 0.0021 | 0.0019 |
| 22 | 0.1333 | 0.0084 | 0.0010 | 0.0020 | 0.0019 |
| 23 | 0.1095 | 0.0108 | 0.0037 | 0.0017 | 0.0014 |
| 26 | 0.0992 | 0.0014 | 0.0119 | 0.0167 | 0.0095 |
| 27 | 0.0990 | 0.0009 | 0.0129 | 0.0091 | 0.0052 |
| 28 | 0.0912 | 0.0106 | 0.0120 | 0.0013 | 0.0014 |
| 30 | 0.1081 | 0.0005 | 0.0155 | 0.0014 | 0.0013 |
| 31 | 0.1109 | 0.0003 | 0.0101 | 0.0019 | 0.0010 |
| 32 | 0.1057 | 0.0003 | 0.0085 | 0.0014 | 0.0009 |
| 33 | 0.1231 | 0.0163 | 0.0042 | 0.0015 | 0.0012 |
| 34 | 0.0889 | 0.0054 | 0.0175 | 0.0016 | 0.0010 |
| 35 | 0.0689 | 0.0003 | 0.0253 | 0.0026 | 0.0012 |
| 36 | 0.2377 | 0.0266 | 0.0053 | 0.0026 | 0.0013 |
| 39 | 0.1238 | 0.0118 | 0.0318 | 0.0041 | 0.0018 |
| 40 | 0.1223 | 0.0186 | 0.0120 | 0.0032 | 0.0017 |
| 41 | 0.1448 | 0.0200 | 0.0061 | 0.0058 | 0.0058 |
| 42 | 0.1090 | 0.0004 | 0.0221 | 0.0057 | 0.0044 |
| 43 | 0.1102 | 0.0191 | 0.0007 | 0.0031 | 0.0015 |
| 44 | 0.1040 | 0.0005 | 0.0082 | 0.0026 | 0.0012 |
| 45 | 0.1105 | 0.0006 | 0.0124 | 0.0014 | 0.0013 |
| 46 | 0.0909 | 0.0124 | 0.0022 | 0.0016 | 0.0011 |
| 47 | 0.1227 | 0.0226 | 0.0054 | 0.0017 | 0.0010 |
| 48 | 0.1515 | 0.0316 | 0.0071 | 0.0025 | 0.0010 |
| 49 | 0.1327 | 0.0197 | 0.0065 | 0.0023 | 0.0013 |
| 51 | 0.0966 | 0.0011 | 0.0425 | 0.0033 | 0.0014 |
| 52 | 0.1684 | 0.0283 | 0.0184 | 0.0040 | 0.0023 |
| 53 | 0.2009 | 0.0204 | 0.0021 | 0.0058 | 0.0035 |
| 54 | 0.1729 | 0.0245 | 0.0100 | 0.0025 | 0.0024 |

| | | | | | |
|----|--------|--------|--------|--------|--------|
| 55 | 0.1424 | 0.0133 | 0.0032 | 0.0023 | 0.0015 |
| 56 | 0.1219 | 0.0003 | 0.0104 | 0.0015 | 0.0011 |
| 58 | 0.1080 | 0.0051 | 0.0097 | 0.0036 | 0.0023 |
| 59 | 0.1419 | 0.0072 | 0.0102 | 0.0016 | 0.0011 |
| 60 | 0.1768 | 0.0216 | 0.0017 | 0.0020 | 0.0019 |
| 61 | 0.1463 | 0.0178 | 0.0006 | 0.0025 | 0.0011 |
| 62 | 0.1298 | 0.0286 | 0.0015 | 0.0024 | 0.0012 |
| 63 | 0.1423 | 0.0105 | 0.0059 | 0.0024 | 0.0012 |
| 64 | 0.1064 | 0.0004 | 0.0243 | 0.0020 | 0.0009 |
| 65 | 0.1747 | 0.0035 | 0.0092 | 0.0018 | 0.0012 |
| 67 | 0.1135 | 0.0100 | 0.0003 | 0.0026 | 0.0013 |
| 68 | 0.1239 | 0.0077 | 0.0002 | 0.0018 | 0.0012 |
| 69 | 0.1088 | 0.0012 | 0.0119 | 0.0048 | 0.0011 |
| 70 | 0.1036 | 0.0191 | 0.0010 | 0.0140 | 0.0063 |

III. References

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- ² N. A. Lakomek, S. Penzel, A. Lends, R. Cadalbert, M. Ernst, and B. H. Meier, *Chemistry* **23** (39), 9425 (2017).